

11. Lubrication

11.1 Purpose of lubrication

The purpose of rolling bearing lubrication is to prevent direct metallic contact between the various rolling and sliding elements. This is accomplished through the formation of a thin oil (or grease) film on the contact surfaces. Lubricant is necessary for operating rolling bearings. For rolling bearings, lubrication has the following advantages:

- (1) **Reduction of friction and wear**
It prevents direct metallic contact between the rolling and sliding elements of bearing components and reduces friction and wear.
- (2) **Prolonged bearing life**
The rolling fatigue life is prolonged by forming an oil film on the rolling contact surface part.
- (3) **Friction heat dissipation** and cooling
circulating lubrication can dissipate heat generated from friction or conducted from the outside.
- (4) Others
It **prevents foreign materials from entering** inside the bearing and suppresses corrosion (rust) by covering the bearing surface with oil.

In order to exhibit these effects, a lubrication method that matches service conditions is required. In addition to this, a quality lubricant must be selected, the proper amount of lubricant must be used and the bearing must be designed to prevent foreign matter from getting in or lubricant from leaking out. If lubrication is insufficient, friction is not reduced, causing excessive rise in bearing temperature or abnormal wear. Therefore, an appropriate lubrication and lubrication method should be selected.

Fig. 11.1 shows the relationship between oil volume, friction loss, and temperature rise. Table 11.1 details the characteristics of this relationship.

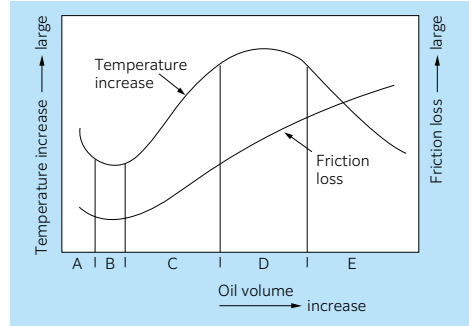


Fig. 11.1

Table 11.1 Oil volume, friction loss, and temperature increase (See Fig. 11.1)

| Range | Characteristics | Lubrication method |
|-------|---|---|
| A | When oil volume is extremely low, direct metallic contact occurs in places between the rolling elements and raceway surfaces. Bearing abrasion and seizing may occur. | — |
| B | A thin oil film develops over all surfaces, friction is minimal and bearing temperature is low. | Grease lubrication Oil mist Air-oil lubrication |
| C | As oil volume increases, heat buildup is balanced by cooling. | Circulating lubrication |
| D | Regardless of oil volume, temperature increases at a fixed rate. | Circulating lubrication |
| E | As oil volume increases, cooling dominates and bearing temperature decreases. | Forced circulation lubrication Oil jet lubrication |

11.2 Lubrication methods and characteristics

Lubrication methods for bearings can be roughly divided into **grease** and **oil lubrication**. Each of these has its own features, so the lubrication method that best offers the required function must be selected.

Characteristics of each method are shown in **Table 11.2**.

Table 11.2 Comparison of grease lubrication and oil lubrication characteristics

| Concern | Method | Grease lubrication | Oil lubrication |
|---------------------------|--------|--------------------|---------------------------|
| Handling | | ◎ | △ |
| Reliability | | ○ | ◎ |
| Cooling effect | | × | ○ (Circulation necessary) |
| Seal structure | | ○ | △ |
| Power loss | | ○ | ○ |
| Environment contamination | | ○ | △ |
| High speed rotation | | × | ○ |

◎ : Very good ○ : Good △ : Fair × : Poor

11.3 Grease lubrication

Grease lubricants are relatively easy to handle and require only the simplest sealing devices. For these reasons, grease is the most widely used lubricant for rolling bearings. It is used in a bearing that is pre-sealed with grease (sealed/shielded bearing), or if using an unsealed bearing, fill the bearing and housing with the proper amount of grease, and replenish or change the grease regularly.

With sealed bearings, the proper grease amount does not cause leakage; however, under use conditions including a lot of vibrations, which cause grease to flow easily, or under high-speed outer ring rotation, in which large centrifugal force is applied on the grease, the grease may purge (in rare cases). Please consult NTN Engineering.

11.3.1 Types and characteristics of grease

Lubricating grease is composed of either a mineral base oil or a synthetic base oil. **To this base a thickener and other additives are added.** The properties of all greases are mainly determined by the kind of base oil used and by the combination of thickening agent and various additives. **Table 11.5** shows general grease varieties and characteristics, and **Table 11.6** shows grease brand names and their characteristics. (See pages A-116 and A-117.) As performance characteristics of even the same type of grease will vary widely from brand to brand, **it is necessary to check the manufacturers' data when selecting grease.**

(1) Base oil
Mineral oil or synthetics such as **ester oil, synthetic hydrocarbon oil**, or **ether oil** are used as the base of greases.

Generally, greases with low viscosity base oils are best suited for low temperatures and high speeds; grease using high-viscosity base oil has superior high-temperature and high-load characteristics.

(2) Thickening agents
 Thickening agents are compounded with base oils to maintain the semi-solid state of the grease. Thickening agents consist of two types of bases: metallic soaps and non-soaps. Metallic soap thickeners include: **lithium, sodium, calcium**, etc. Non-soap base thickeners are divided into two groups: inorganic (**silica gel, bentonite**, etc.) and organic (**polyurea, fluorocarbon**, etc.). The various special characteristics of a grease, such as **limiting temperature range, mechanical stability**, water resistance, etc. depend largely on the type of **thickening agent** used. For example, a sodium based grease is generally poor in water resistance properties, while greases with bentone, poly-urea and other non-metallic soaps as

the thickening agent are generally superior in high temperature properties.
 (3) Additives
 Various additives are added to grease depending on the purpose. Typical additives include **anti-oxidants, high-pressure additives** (EP additives), **rust preventives**, and **anti-corrosives**. For bearings subject to heavy loads and/or shock loads, grease containing high-pressure additives should be used. Anti-oxidants are added to grease used in most types of rolling bearings.

(4) Consistency
 Consistency is an index that indicates hardness and fluidity of grease. **The higher the NLGI number, the HARDER the grease is.** For the lubrication of rolling bearings, greases with the NLGI consistency numbers of 1, 2, and 3 are used. General relationships between consistency and application of grease are shown in **Table 11.3**.

Table 11.3 Consistency of grease

| NLGI consistency No. | JIS(ASTM) 60 times blend consistency | Application |
|----------------------|--------------------------------------|---|
| 0 | 355 to 385 | For centralized greasing use |
| 1 | 310 to 340 | For centralized greasing use |
| 2 | 265 to 295 | For general use and sealed bearing use |
| 3 | 220 to 250 | For general use, high temperature use, and sealed bearing use |
| 4 | 175 to 205 | For special use |

(5) Mixing different types of greases
 When greases of different kinds are mixed together, the consistency of the greases will change (usually softer), the operating temperature range will be lowered, and other changes in characteristics will occur. **As a rule, grease should not be mixed with grease of any other brand.** However, if different greases must be mixed, at least greases with the same base oil and thickening agent should be selected.

11.3.2 Amount of grease

The amount of grease used in any given situation will depend on many factors relating to the size and shape of the housing, space limitations, bearing's rotating speed and type of grease used. As a rule of thumb, **bearings should be filled to 30 to 40% of their space and housing should be filled 30 to 60%**. Where speeds are high and temperature rises need to be kept to a minimum, a reduced amount of grease should be used. Excessive amounts of grease cause temperature rises which in turn cause the grease to soften and may allow leakage. Oxidation and deterioration of excessive grease fills may cause the lubricating efficiency to be lowered. Moreover, the standard bearing space can be found by formula (11.1)

$$V = K \cdot W \dots\dots\dots (11.1)$$

where,

V : Quantity of bearing space open type (approx.), cm³

K : Bearing space factor (see value of K in **Table 11.4**)

W : Mass of bearing, kg

A predetermine amount of grease is filled in the bearing with a grease gun or a syringe. After sealing it is not possible to spread the grease by hand - only by rotating the bearing by hand.

Table 11.4 Bearing space factor K

| Bearing type ¹⁾ | | Cage type | K | |
|--|----------------------------------|-----------------------|-------------------|----|
| Deep groove ball bearing ²⁾ | | Pressed cage | 61 | |
| Angular contact ball bearing | | Pressed cage | 54 | |
| | | Machined cage | 33 | |
| | | Molded resin cage | 33 | |
| Cylindrical roller bearing | NU type ³⁾ | Pressed cage | 50 | |
| | | Machined cage | 36 | |
| | N type ⁵⁾ | Pressed cage | 55 | |
| | | Machined cage | 37 | |
| | ULTAGE series(EA type) E type | NU type ⁴⁾ | Machined cage | 33 |
| | | | Molded resin cage | 33 |
| | | N type ⁴⁾ | Machined cage | 34 |
| | | | Molded resin cage | 35 |
| Tapered roller bearing | | Pressed cage | 46 | |
| Spherical roller bearing | Type C | | Pressed cage | 35 |
| | Type B Type 213 | | Machined cage | 28 |
| | ULTAGE series | Type EA | Pressed cage | 33 |
| | | Type EM | Machined cage | 31 |

1) Does not apply to model numbers that are not specified in the catalog.
 2) Does not apply top 160 series bearings. 3) Does not apply to NU4 series.
 4) Applies to G1 machined cages only. 5) Does not apply to N4 series.

Table 11.5 Grease varieties and characteristics ¹⁾

| | Soap-based | | | | |
|---------------------------------|--|--|--|--|------------------------------------|
| | Lithium (Li) grease | | | Calcium (Ca) grease | |
| Thickening agent ²⁾ | Li soap | | | Li complexed soap | Ca soap (cup grease) |
| Base oil ³⁾ | Mineral oil | Ester oil | Silicone oil | Mineral oil | Mineral oil |
| Dropping point °C | 170 to 190 | 170 to 190 | 200 to 210 | >250 | 80 to 100 |
| Operating temperature range °C | -30 to 120 | -50 to 130 | -50 to 160 | -30 to 130 | -20 to 70 |
| Mechanical stability | Good | Good | Good | Good | OK |
| Pressure resistance | Good | Good | Poor | Good | OK |
| Water resistance | Good | Good | Good | Good | Good |
| Characteristics/ application | Balanced performance with less disadvantages | Excellent low temperature and wear characteristics | Excellent characteristics at low and high temperatures | Balanced performance with less disadvantages | Used for low speed and light loads |
| | All purpose grease | Suitable for small sized and miniature bearings | Poor load resistance | Usable for relatively high temperature | Unusable for high temperature |

- 1) Use the grease performance as rough standards because it differs depending on the manufacturer's additive formation.
- 2) Na soap-based grease may be emulsified by water and high humidity conditions.
Urea-based grease may deteriorate polyfluorocarbons and rubber.

Table 11.6 Grease brands and their nature

| Brand | Code | Thickener | Base oil | Base oil viscosity mm ² /s | |
|-----------------------|------|-------------------|-----------------------|---------------------------------------|-------|
| | | | | 40°C | 100°C |
| Alvania Grease S2 | 2AS | Li soap | Mineral oil | 131 | 12.2 |
| Alvania Grease S3 | 3AS | Li soap | Mineral oil | 131 | 12.2 |
| Alvania EP Grease 2 | 8A | Li soap | Mineral oil | 220 | 15.9 |
| Multemp PS No. 2 | 1K | Li soap | Ester + PAO | 15.9 | — |
| Multemp SRL | 5K | Li soap | Ester | 24.1 | — |
| SH33L | 3L | Li soap | Silicone | 70 | 27 |
| SH44M | 4M | Li soap | Silicone | 80 | 19 |
| ISOFLEX NBU15 | 15K | Ba complexed soap | Diester + mineral oil | 23 | 5 |
| SHC POLYREX 462 | L791 | Urea | PAO | 460 | 40 |
| SE-1 | L749 | Urea | PAO + ester | 22 | 5 |
| ME-1 | L700 | Urea | Ester + PAO | 61.3 | 9.3 |
| EP-1 | L542 | Urea | PAO | 46.8 | — |
| NA103A | L756 | Urea | PAO + ether | 53.5 | — |
| MP-1 | L448 | Urea | Synthetic oil | 40.6 | 7.1 |
| Grease J | L353 | Urea | Ester | 75 | 10 |
| Cosmo Wide Grease WR3 | 2M | Na terephthalate | Diester + mineral oil | 31.6 | 6 |
| Mobilgrease 28 | 9B | Bentonite | PAO | 30 | 5.7 |
| Aeroshell Grease 7 | 5S | Microgel | Diester | 10.3 | 3.1 |

- Note: 1. Representative values are shown for the base oil viscosity, consistency, and dropping point.
- 2. The upper and lower limits of the operating temperature range differ depending on the usage environment and requirement specifications. Please consult with NTN Engineering.

| Soap-based | | Non-soap-based | | | |
|-------------------------------|--|--|---|---|--|
| Calcium (Ca) grease | Sodium (Na) grease | Organic | | | Inorganic |
| Ca complexed soap | Na soap | Urea | Urea | PTFE | Silica gel |
| Mineral oil | Mineral oil | Mineral oil | Synthetic oil | Fluorinated | Ester oil |
| 200 to 280 | 170 to 200 | >260 | >260 | None | >260 |
| -20 to 130 | -20 to 130 | -30 to 140 | -40 to 180 | -40 to 250 | -70 to 150 |
| Good | Good | Good to Excellent | Good to Excellent | OK to Good | Good |
| Good to Excellent | Good | Good to Excellent | Good to Excellent | Good | Good |
| Good | Poor | Good to Excellent | Good to Excellent | Good | Good |
| Excellent pressure resistance | Some emulsification when water is introduced Usable for relatively high temperature | Excellent water resistance and oxidation stability | Excellent water resistance and oxidation stability Used for high temperature and high speed applications | Excellent chemical resistance Used for high temperature applications | Excellent characteristics at low temperature |

- 3) Ester oil-based grease may swell acrylic materials, and silicone-based grease may swell silicone materials.
Some silicone-based greases and fluorine-based greases have poor noise performance and rustproofing performance.

| 60 times blend consistency | | Dropping point °C | Operating temperature range °C | Characteristics |
|----------------------------|---------|-------------------|--------------------------------|---|
| Representative value | NLGI No | | | |
| 283 | 2 | 181 | -25 to 120 | All-purpose (standard grease for deep grease ball bearings) |
| 242 | 3 | 182 | -20 to 135 | All-purpose (standard grease for ball bearings of bearing units) |
| 284 | 2 | 184 | -20 to 110 | All-purpose for high loads |
| 270 | 2 | 190 | -50 to 130 | For low temperature and low torque |
| 250 | 2 to 3 | 192 | -40 to 150 | For low temperature to high temperature, all-purpose (standard grease for miniature/small diameter ball bearings) |
| 320 | 1 to 2 | 220 | -70 to 140 | For low temperature |
| 260 | 2 to 3 | 204 | -40 to 160 | For high temperature |
| 280 | 2 | 220 or above | -40 to 130 | For high speed |
| 280 | 2 | 270 | -20 to 170 | For food machinery |
| 265 | 2 | 220 or above | -50 to 120 | For high speed |
| 231 | 3 | 250 or above | -30 to 160 | For high temperature and high speed |
| 220 | 2 | 260 or above | -40 to 160 | For high temperature and high speed |
| 270 | 2 | 260 or above | -40 to 180 | Brittle separation |
| 243 | 3 | 250 or above | -40 to 150 | For high temperature and high speed |
| 305 | 1 to 2 | 280 or above | -20 to 180 | For high temperature |
| 238 | 3 | 230 or above | -40 to 150 | For low temperature to high temperature, all-purpose |
| 293 | 1 to 2 | 307 | -54 to 177 | MIL-PRF-81322 For low temperature to high temperature |
| 296 | 1 to 2 | 260 or above | -73 to 149 | MIL-PRF-23827C |

11.3.3 Grease replenishment

As the lubricating performance of grease declines with the time, grease must be filled in proper intervals.

The replenishment interval depends on the type of bearing, dimensions, bearing's rotating speed, bearing temperature, and type of grease.

An easy reference chart for calculating grease replenishment interval is shown in Fig. 11.2.

This chart indicates the replenishment interval

for standard rolling bearing grease when used under normal operating conditions. As operating temperatures increase, the grease interval should be shortened accordingly. Generally, for every 10°C increase in bearing temperature above 80°C, the grease interval period is shortened to "2/3".

For grease replenishment interval of the ULTAGE series, please contact NTN Engineering.

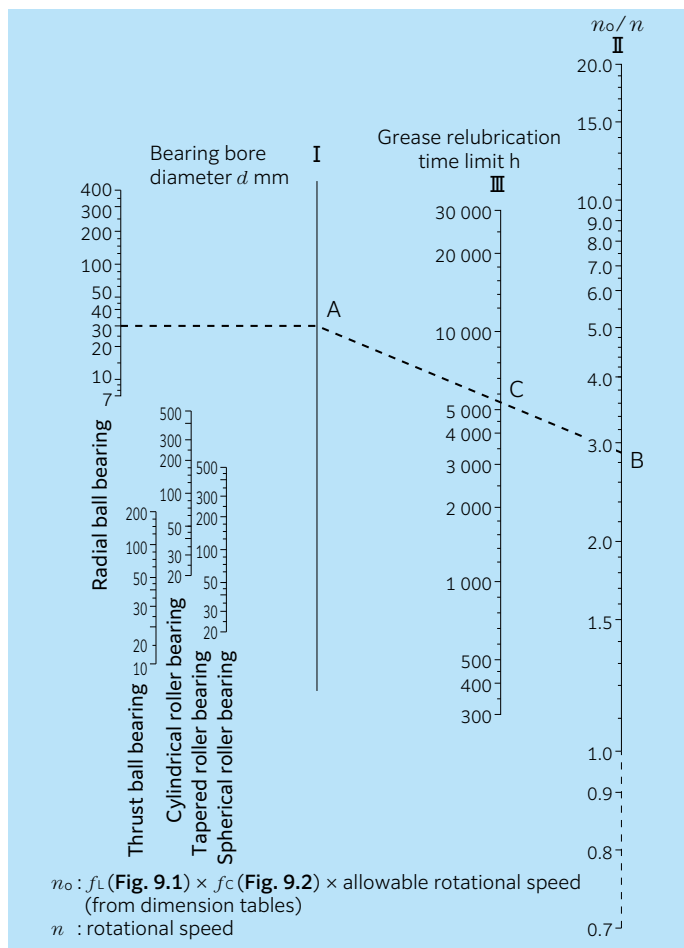


Fig. 11.2 Diagram for grease interval

(Example) Find the grease relubrication time limit for deep groove ball bearing 6206, with a radial load of 2.0 kN operating at 3 600 min⁻¹

From Fig. 9.1 $C_r / P_r = 21.6 / 2.0 \text{ kN} = 10.8$, $f_L = 0.96$. Allowable rotational speed from the dimensions tables for bearing 6206 is 11 000 min⁻¹. Allowable rotational speed n_o for 2.0 kN radial load is:

$$n_o = 0.96 \times 11\,000 = 10\,560 \text{ min}^{-1}$$

$$\text{Therefore, } \frac{n_o}{n} = \frac{10\,560}{3\,600} = 2.93$$

The point where vertical line I intersects a horizontal line drawn from the point equivalent of $d = 30$ for the radial ball bearing shown in Fig. 11.2 shall be point A. Find intersection point C where vertical line III intersects the straight line formed by joining point B ($n_o/n = 2.93$) with A by a straight line II. It shows that grease life in this case is approximately 5,500 hours.

11.3.4 Grease life estimation of sealed ball bearings

There is a method of estimating the grease life of single row sealed and greased ball bearings.

The estimated grease life changes depending on the grease type, temperature, shaft rotational speed, and load; therefore, please contact NTN Engineering for details.

11.4 Solid grease

"Solid grease" is a lubricant composed mainly of lubricating grease and ultra-high polymer polyethylene. Solid grease begins as grease that has the same viscosity as a more traditional grease. After being heated and cooled, a process known as a "calcination", the grease hardens while maintaining a large quantity of lubricant within the polymer structure. The result of this solidification is that the grease does not easily leak from the bearing, even when the bearing is subjected to strong vibrations or centrifugal force.

Bearings with solid grease are available in two types: the spot-pack type in which solid grease is injected into the cage, and the full-pack type in which all free space around the rolling elements is completely filled with solid grease.

Spot-pack solid grease is available for deep groove ball bearings, small diameter ball bearings, and bearing units. Full-pack solid grease is available for self-aligning ball bearings, spherical roller bearings, and needle roller bearings.

Primary advantages:

- (1) Minimal grease leakage
- (2) Low bearing torque with spot-pack type solid grease

For more details, please refer to the special catalog "Bearings with solid grease (CAT. No. 3022/E)."

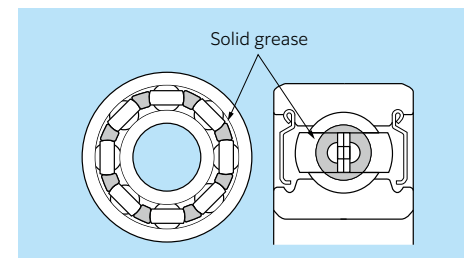


Fig. 11.3 Deep groove ball bearing with spot-pack solid grease (Z shield) (Available for deep groove ball bearings)

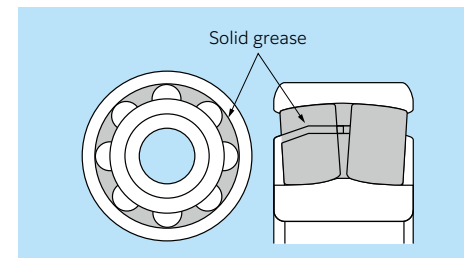


Fig. 11.4 Spherical roller bearing with full-pack solid grease (Available for spherical roller bearings)

11.5. Oil lubrication

Oil lubrication is suitable for applications requiring that bearing-generated heat or heat applied to the bearing from other sources be

carried away from the bearing and dissipated to the outside.

Table 11.7 shows the main methods of oil lubrication.

Table 11.7 Oil lubrication methods

| Lubrication method | Example | Lubrication method | Example |
|---|---------|--|---------|
| <p>(Oil bath lubrication)</p> <ul style="list-style-type: none"> Oil bath lubrication is the most generally used method of lubrication, and is widely used for low to moderate rotational speed applications. For horizontal shaft applications, oil level should be maintained at approximately the center of the lowest rolling element, according to the oil gauge, when the bearing is at rest. For vertical shafts at low speeds, oil level should be maintained at 50 - 80% submergence of the rolling elements. | | <p>(Disc lubrication)</p> <ul style="list-style-type: none"> In this method, a partially submerged disc rotates and pulls oil up into a reservoir from which it then drains down through the bearing, lubricating it. | |
| <p>(Oil spray lubrication)</p> <ul style="list-style-type: none"> In this method, an impeller or similar device mounted on the shaft draws up oil and sprays it onto the bearing. This method can be used at considerably high speeds. | | <p>(Oil mist lubrication)</p> <ul style="list-style-type: none"> Using pressurized air, lubricating oil is atomized before passing through the bearing. Due to the low lubricant resistance, this method is well suited to high speed applications. | |
| <p>(Drip lubrication)</p> <ul style="list-style-type: none"> In this method, oil is collected above the bearing and allowed to drip down into the housing where it becomes a lubricating mist as it strikes the rolling elements. Another version allows only slight amounts of oil to pass through the bearing. Used at relatively high speeds for light to moderate load applications. In most cases, oil volume is a few drops per minute. | | <p>(Air-oil lubrication)</p> <ul style="list-style-type: none"> In this method, the required minimum amount of lubricating oil is measured and fed to each bearing at ideal intervals using compressed air. Fresh lubricating oil is constantly fed. Because the required oil quantity is very small, the working environment can be kept clean. | |
| <p>(Circulating lubrication)</p> <ul style="list-style-type: none"> Used for bearing cooling or for automatic oil supply systems in which the oil supply is centrally located. One of the advantages of this method is that oil cooling devices and filters to maintain oil purity can be installed within the system. In order for oil to thoroughly lubricate the bearing, oil inlets and outlets must be provided on opposite sides of the bearing. | | <p>(Oil jet lubrication)</p> <ul style="list-style-type: none"> This method lubricates by injecting oil under high pressure directly into the side of the bearing. This is a reliable system for high speed, high temperature or otherwise severe conditions. Used for lubricating the bearings in jet engines, gas turbines, and other high speed equipment. Under-race lubrication is one example of this type of lubrication. | |

11.5.1 Selection of lubricating oil

Under normal operating conditions, machine oil, turbine oil, and other mineral oils are widely used for the lubrication of rolling bearings.

However, for temperatures below -30°C or above 150°C, synthetic oils such as ester oil, silicone oil, and fluorinated oil are used.

For lubricating oils, viscosity is one of the most important properties and determines an oil's lubricating efficiency. If viscosity is too low, formation of the oil film will be insufficient, and damage to the rolling surface will occur.

If viscosity is too high, viscous resistance will also be great, resulting in temperature increase and friction loss. In general, for higher speed applications, a lower viscosity oil should be used; for heavier load applications, a higher viscosity oil should be used.

Lubrication of rolling bearings requires viscosity shown in Table 11.8, which is dependent on the use conditions. Fig 11.5 shows the relation between lubricating oil viscosity and temperature. This is used to select a lubrication oil with viscosity characteristics appropriate for the operating temperature.

For reference, Table 11.9 lists the selection standards for lubricating oil viscosity based on bearing operating conditions.

Table 11.8 Required lubricating oil viscosity for bearings

| Bearing type | Dynamic viscosity mm ² /s |
|---|--------------------------------------|
| Ball bearings, Cylindrical roller bearings, Needle roller bearings | 13 or above |
| Spherical roller bearings, Tapered roller bearings, Needle roller thrust bearings | 20 or above |
| Self-aligning roller thrust bearing | 30 or above |

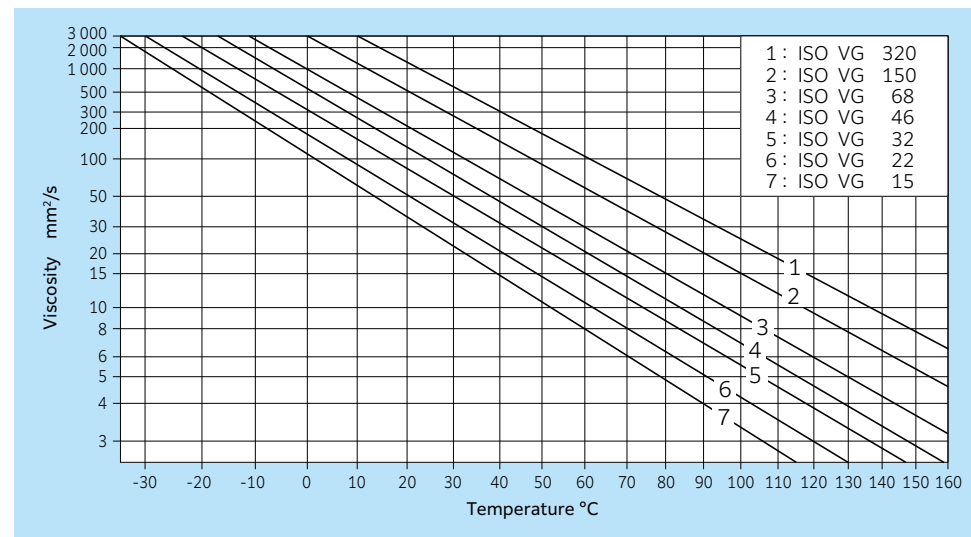


Fig 11.5 Relation between lubricating oil viscosity and temperature

Table 11.9 Standards for lubricating oil viscosity

| Bearing operating temperature °C | dn value ¹⁾ | Lubricating oil ISO viscosity grade (VG) | | Suitable bearing |
|----------------------------------|----------------------------------|--|--------------------------|--|
| | | Normal load | Heavy load or shock load | |
| -30 to 0 | Up to allowable rotational speed | 22, 32 | 46 | All types |
| 0 to 60 | Up to 15 000 | 46, 68 | 100 | All types |
| | 15 000 to 80 000 | 32, 46 | 68 | All types |
| | 80 000 to 150 000 | 22, 32 | 32 | All types but thrust ball bearings |
| | 150 000 to 500 000 | 10 | 22, 32 | Single row radial ball bearings, cylindrical roller bearings |
| 60 to 100 | Up to 15 000 | 150 | 220 | All types |
| | 15 000 to 80 000 | 100 | 150 | All types |
| | 80 000 to 150 000 | 68 | 100, 150 | All types but thrust ball bearings |
| | 150 000 to 500 000 | 32 | 68 | Single row radial ball bearings, cylindrical roller bearings |
| 100 to 150 | Up to allowable rotational speed | 320 | | All types |
| 0 to 60 | Up to allowable rotational speed | 46, 68 | | Self-aligning roller bearing |
| 60 to 100 | Up to allowable rotational speed | 150 | | |

1) dn value: [dn = bearing bore diameter d (mm) × rotational speed n (mm⁻¹)]
 Note: 1. Applied when lubrication method is either oil bath or circulating lubrication.
 2. Please consult NTN Engineering in cases where operating conditions fall outside the range covered by this table.

11.5.2 Oiling amount

When a bearing is to be supplied with oil forcibly, the amount of heat generated from the bearing is equal to the sum of the amount of heat dissipated from the housing and the amount of heat carried away by the oil.

The oiling amount that serves as a rough indication when a standard housing is used can be obtained by formula (11.2).

$$Q = K \cdot q \dots\dots\dots(11.2)$$

where,

Q: oiling amount per bearing (cm³/min)

K: coefficient determined by allowable temperature rise of oil (Table 11.10)

q: oiling amount obtained by diagram (cm³/min) (Fig. 11.6)

The heat dissipation amount differs depending on the housing type. Therefore, in the actual operation, it is desirable to obtain the oiling amount suitable for the actual machine by adjusting the amount obtained by formula (11.2) to 1.5 to 2 times.

In addition, when calculating the oiling amount assuming that no heat is dissipated from the housing and the generated heat

amount is completely carried away by the oil, use the shaft diameter in the diagram as d = 0.

Table 11.10 Value of K

| Expelled oil temp minus supplied oil temp °C | K |
|--|------|
| 10 | 1.5 |
| 15 | 1 |
| 20 | 0.75 |
| 25 | 0.6 |

(Example) For tapered roller bearing 30220U mounted on a flywheel shaft with a radial load of 9.5 kN, operating at 1 800 min⁻¹, what is the amount of lubricating oil Q required to keep the bearing temperature rise below 15°C?

d = 100mm,
 dn = 100 × 1 800 = 18 × 10⁴
 From Fig. 11.6 q = 180cm³/min
 Assume the bearing temperature is approximately equal to the expelled oil temperature,
 from Table 11.10, since K = 1
 Q = K × q = 1 × 180 = 180cm³/min

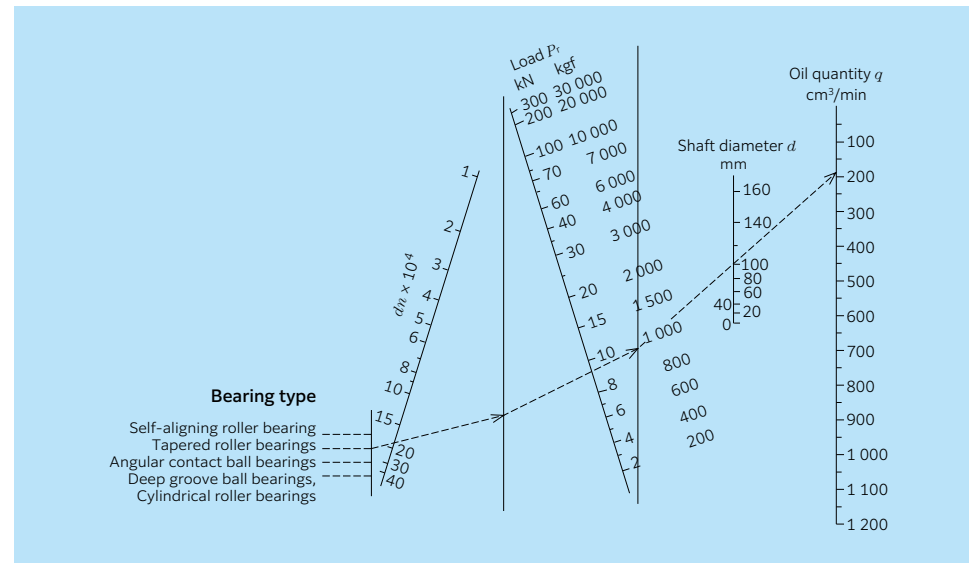


Fig. 11.6 Oil quantity guidelines

11.5.3 Relubrication intervals

The intervals at which lubricating oil should be changed varies depending upon operating conditions, oil quantity, and type of oil used. In general, for oil bath lubrication where the operating temperature is 50°C or less, oil should be replaced once a year. When the operating temperature is between 80°C - 100°C, oil should be replaced at least once every three months. For important equipment, it is advisable that lubricating efficiency and oil purity deterioration be checked regularly to determine when oil replacement is necessary.